

# A LOCALLY DIVERGENCE-FREE LOCAL CHARACTERISTIC DECOMPOSITION BASED PATH-CONSERVATIVE CENTRAL-UPWIND SCHEME FOR IDEAL MAGNETOHYDRODYNAMICS\*

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**Abstract.** We introduce a locally divergence-free local characteristic decomposition based path-conservative central-upwind (LCD-PCCU) scheme for ideal magnetohydrodynamics (MHD) equations. The proposed method is a low-dissipation extension of the recently proposed locally divergence-free PCCU scheme. To reduce the numerical dissipation, we incorporate the LCD into the PCCU framework. The resulting LCD-PCCU method enhances the resolution of numerical solutions as demonstrated through a series of benchmark tests.

**Key words.** Ideal magnetohydrodynamics, divergence-free constraints, local characteristic decomposition, path-conservative central-upwind scheme.

**MSC codes.** 65M08, 76W05, 76M12, 35L65

**1. Introduction.** This paper focuses on the development of a novel and low-dissipation numerical method for ideal magnetohydrodynamics (MHD) equations, which play a central role in modeling a wide range of physical phenomena in astrophysics, plasma physics, space physics, and engineering. These models describe the dynamics of electrically conducting fluids interacting with magnetic fields and consist of hyperbolic systems of partial differential equations (PDEs) that couple fluid flow with electromagnetic effects. A crucial property of these models is a constraint on the magnetic field, which has to remain divergence-free if it is divergence-free initially. Numerically, however, this condition is nontrivial to maintain, and improperly handling the divergence-free constraint at the discrete level can lead to numerical instabilities or the development of nonphysical structures in the solution; see, e.g., [3, 4, 25, 36].

Over the past decades, numerous approaches have been developed to address the divergence-free constraint. Among them are the projection method (see, e.g., [4]), the constrained transport (CT) method (see, e.g., [3, 11, 15, 17, 19, 23, 29, 35, 37]), locally divergence-free discontinuous Galerkin [25, 38] and finite-volume [9, 10] methods (these methods maintain zero divergence within each computational cell), and globally divergence-free high-order finite-volume and discontinuous Galerkin methods; see, e.g., [1, 2, 16, 18, 26, 27].

Alternatively, instead of enforcing the divergence-free constraint explicitly, one can reduce divergence errors through the inclusion of additional Godunov-Powell terms. This leads to the so-called eight-wave formulation of the ideal MHD equations; see, e.g., [20, 31–33]. This formulation introduces nonconservative source terms proportional to the divergence of the magnetic field. Although these terms vanish analytically, they help to control numerical divergence errors by advecting them with the flow and preventing their accumulation. Moreover, the modified system gains important properties such as Galilean invariance and entropy symmetrizability, making it well-suited for the development of entropy-stable schemes; see,

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35 e.g., [7, 14, 28, 31–33].

36 In [9], the Godunov-Powell modification of the ideal MHD and shallow water MHD equations was  
 37 utilized to develop a locally divergence-free second-order semi-discrete path-conservative central-upwind  
 38 (PCCU) scheme, which was later extended to the magnetic rotating shallow water model in [10]. In [9],  
 39 the studied systems were augmented by evolution equations for the spatial derivatives of the magnetic field  
 40 components, and the resulting systems were numerically solved by a PCCU scheme, which was originally  
 41 developed in [6] as a “black-box” solver for general nonconservative hyperbolic systems. We stress that  
 42 the PCCU schemes are, like any central and central-upwind (CU) schemes, Riemann-problem-solver-free,  
 43 and at the same time, they are designed to handle the nonconservative product terms across cell interfaces  
 44 in a stable manner.

45 Although the PCCU scheme for the ideal MHD system [9] is quite accurate, efficient, and robust, its  
 46 resolution can be further improved by reducing the amount of numerical dissipation. This can be done  
 47 with the help of the local characteristic decomposition (LCD) based PCCU (LCD-PCCU) scheme, which  
 48 was recently introduced in [12] as an extension of the LCD-based CU (LCD-CU) scheme proposed in [8]  
 49 for hyperbolic systems of conservation laws. Compared with the CU and PCCU schemes, the LCD-CU  
 50 and LCD-PCCU schemes achieve higher resolution by aligning the numerical flux computation with the  
 51 characteristic structure of the system; see [8, 12, 13]. In this paper, we develop the LCD-PCCU scheme  
 52 for the ideal MHD equations and test it on a number of numerical experiments, which confirm that the  
 53 proposed scheme achieves high resolution, while being robust and positivity-preserving, and effectively  
 54 maintaining divergence control. The obtained numerical results also demonstrate that the new scheme  
 55 outperforms the PCCU scheme from [9].

56 The rest of the paper is organized as follows. In §2, we present the Godunov-Powell modification of  
 57 the ideal MHD equations and its augmented form. In §3, we apply the two-dimensional (2-D) LCD-PCCU  
 58 scheme for the studied MHD system. Finally, in §4, we present results of several numerical experiments.

59 **2. Ideal MHD Equations.** The ideal MHD equations read as

$$\begin{aligned}
 & \rho_t + \nabla \cdot (\rho \mathbf{u}) = 0, \\
 & (\rho \mathbf{u})_t + \nabla \cdot \left[ \rho \mathbf{u} \mathbf{u}^\top + \left( p + \frac{1}{2} |\mathbf{b}|^2 \right) I - \mathbf{b} \mathbf{b}^\top \right] = \mathbf{0}, \\
 & \mathcal{E}_t + \nabla \cdot \left[ \left( \mathcal{E} + p + \frac{1}{2} |\mathbf{b}|^2 \right) \mathbf{u} - \mathbf{b} (\mathbf{u} \cdot \mathbf{b}) \right] = 0, \\
 & \mathbf{b}_t - \nabla \times (\mathbf{u} \times \mathbf{b}) = \mathbf{0},
 \end{aligned}
 \tag{2.1}$$

61 where  $t$  is time,  $\rho$  is the density,  $p$  is the pressure,  $\mathbf{u} = (u, v, w)^\top$  is the fluid velocity,  $\mathbf{b} = (b_1, b_2, b_3)^\top$  is  
 62 the magnetic field, and  $\mathcal{E}$  is the total energy. Additionally,  $I$  is the identity matrix and  $\gamma$  is the ratio of  
 63 specific heats. The system (2.1) is completed through the equation of state (EOS)

$$\mathcal{E} = \frac{p}{\gamma - 1} + \frac{\rho}{2} |\mathbf{u}|^2 + \frac{1}{2} |\mathbf{b}|^2.
 \tag{2.2}$$

65 It is easy to show that provided that the magnetic field is initially divergence-free, then the magnetic field  
 66 satisfies

$$\nabla \cdot \mathbf{b} = 0.
 \tag{2.3}$$

68 In this paper, we will develop a new numerical method for the Godunov-Powell modified ideal MHD  
 69 equations, which read as

$$\begin{aligned}
 & \rho_t + \nabla \cdot (\rho \mathbf{u}) = 0, \\
 & (\rho \mathbf{u})_t + \nabla \cdot \left[ \rho \mathbf{u} \mathbf{u}^\top + \left( p + \frac{1}{2} |\mathbf{b}|^2 \right) I - \mathbf{b} \mathbf{b}^\top \right] = -\mathbf{b} (\nabla \cdot \mathbf{b}), \\
 & \mathcal{E}_t + \nabla \cdot \left[ \left( \mathcal{E} + p + \frac{1}{2} |\mathbf{b}|^2 \right) \mathbf{u} - \mathbf{b} (\mathbf{u} \cdot \mathbf{b}) \right] = -(\mathbf{u} \cdot \mathbf{b}) (\nabla \cdot \mathbf{b}), \\
 & \mathbf{b}_t - \nabla \times (\mathbf{u} \times \mathbf{b}) = -\mathbf{u} (\nabla \cdot \mathbf{b}),
 \end{aligned}
 \tag{2.4}$$

71 which is completed through the EOS (2.2). We stress that the system (2.4), (2.2)—unlike the original  
72 system (2.1)–(2.2)—has a complete set of eight eigenvalues with eight corresponding eigenvectors: This  
73 allows for an LCD and thus for designing an LCD-PCCU scheme.

74 As in [9], we restrict our attention to the 2-D case, where all the quantities of interest depend on  
75 the spatial variables  $x$  and  $y$  and time  $t$  only. In this case, the divergence-free condition (2.3) reads as  
76  $(b_1)_x + (b_2)_y = 0$ , and we augment the Godunov-Powell modified ideal MHD system (2.4), (2.2) by adding  
77 the equations for the auxiliary variables  $A := (b_1)_x$  and  $B := (b_2)_y$ :

$$78 \quad (2.5) \quad \begin{aligned} A_t + (uA - b_2 u_y)_x + (vA + b_1 v_x)_y &= 0, \\ B_t + (uB + b_2 u_y)_x + (vB - b_1 v_x)_y &= 0, \end{aligned}$$

79 which are obtained by differentiating the  $b_1$ - and  $b_2$ -equations in (2.1).

80 One can write the system (2.4)–(2.5), (2.2) in the following vector form:

$$81 \quad (2.6) \quad \mathbf{U}_t + \mathbf{F}(\mathbf{U})_x + \mathbf{G}(\mathbf{U})_y = Q^x(\mathbf{U})\mathbf{U}_x + Q^y(\mathbf{U})\mathbf{U}_y,$$

$$82 \quad (2.7) \quad \tilde{\mathbf{U}}_t + \tilde{\mathbf{F}}(\mathbf{W})_x + \tilde{\mathbf{G}}(\mathbf{W})_y = \mathbf{0},$$

83 where

$$84 \quad (2.8) \quad \begin{aligned} \mathbf{U} &= (\rho, \rho u, \rho v, \rho w, b_1, b_2, b_3, \mathcal{E})^\top, \quad \tilde{\mathbf{U}} = (A, B)^\top, \quad \mathbf{W} = (\mathbf{U}^\top, \tilde{\mathbf{U}}^\top)^\top, \\ \mathbf{F}(\mathbf{U}) &= \left( \rho u, \rho u^2 + p + \frac{1}{2}|\mathbf{b}|^2 - b_1^2, \rho uv - b_1 b_2, \rho uw - b_1 b_3, 0, ub_2 - vb_1, \right. \\ &\quad \left. ub_3 - wb_1, \left( \mathcal{E} + p + \frac{1}{2}|\mathbf{b}|^2 \right) u - (\mathbf{u} \cdot \mathbf{b}) b_1 \right)^\top, \\ \mathbf{G}(\mathbf{U}) &= \left( \rho v, \rho uv - b_1 b_2, \rho v^2 + p + \frac{1}{2}|\mathbf{b}|^2 - b_2^2, \rho vw - b_2 b_3, vb_1 - ub_2, 0, \right. \\ &\quad \left. vb_3 - wb_2, \left( \mathcal{E} + p + \frac{1}{2}|\mathbf{b}|^2 \right) v - (\mathbf{u} \cdot \mathbf{b}) b_2 \right)^\top, \\ Q^x(\mathbf{U}) &= \mathbf{q} \mathbf{e}_5^\top, \quad Q^y(\mathbf{U}) = \mathbf{q} \mathbf{e}_6^\top, \quad \mathbf{q} := -(0, b_1, b_2, b_3, u, v, w, \mathbf{u} \cdot \mathbf{b})^\top, \\ \tilde{\mathbf{F}}(\mathbf{W}) &= (uA - b_2 u_y, uB + b_2 u_y)^\top, \quad \tilde{\mathbf{G}}(\mathbf{W}) = (vA + b_1 v_x, vB - b_1 v_x)^\top, \end{aligned}$$

85 and  $\mathbf{e}_5$  and  $\mathbf{e}_6$  are the fifth and sixth unit vectors in  $\mathbb{R}^8$ , respectively.

86 Note that for smooth solutions, the system (2.4), (2.2) can be rewritten in an equivalent quasi-linear  
87 form:

$$88 \quad (2.9) \quad \mathbf{U}_t + C^x(\mathbf{U})\mathbf{U}_x + C^y(\mathbf{U})\mathbf{U}_y = \mathbf{0},$$

89 where the matrices  $C^x(\mathbf{U})$  and  $C^y(\mathbf{U})$  are specified in Appendix A. Furthermore, one can switch to the  
90 primitive variables  $\mathbf{V} = (\rho, u, v, w, p, b_1, b_2, b_3)^\top$  and rewrite the system (2.9) in a different quasi-linear  
91 form:

$$92 \quad (2.10) \quad \mathbf{V}_t + D^x(\mathbf{V})\mathbf{V}_x + D^y(\mathbf{V})\mathbf{V}_y = \mathbf{0},$$

93 where the matrices  $D^x(\mathbf{V})$  and  $D^y(\mathbf{V})$  are specified in Appendix B. In the following, we will use the forms  
94 (2.9) and (2.10) to design the LCD-CU numerical fluxes and to perform a piecewise linear reconstruction,  
95 respectively.

96 **3. 2-D Flux Globalization Based LCD-PCCU Scheme.** In this section, we apply the 2-D flux  
97 globalization based LCD-PCCU scheme from [12] to the studied augmented ideal MHD system (2.6)–(2.8).  
98 To this end, we first rewrite the system (2.6) in the following quasi-conservative form:

$$99 \quad (3.1) \quad \mathbf{U}_t + \mathbf{K}(\mathbf{U})_x + \mathbf{L}(\mathbf{U})_y = \mathbf{0}, \quad \mathbf{K}(\mathbf{U}) = \mathbf{F}(\mathbf{U}) - \mathbf{I}^x(\mathbf{U}), \quad \mathbf{L}(\mathbf{U}) = \mathbf{G}(\mathbf{U}) - \mathbf{I}^y(\mathbf{U}),$$

100 where

$$101 \quad \mathbf{I}^x(\mathbf{U}) := \int_{\hat{x}}^x [Q^x(\mathbf{U})\mathbf{U}_\xi(\xi, y, t)] d\xi, \quad \mathbf{I}^y(\mathbf{U}) := \int_{\hat{y}}^y [Q^y(\mathbf{U})\mathbf{U}_\eta(x, \eta, t)] d\eta,$$

102 with  $\hat{x}$  and  $\hat{y}$  being arbitrary numbers.

We cover the computational domain with uniform cells  $C_{j,k} := [x_{j-\frac{1}{2}}, x_{j+\frac{1}{2}}] \times [y_{k-\frac{1}{2}}, y_{k+\frac{1}{2}}]$  centered at  $(x_j, y_k) = ((x_{j-\frac{1}{2}} + x_{j+\frac{1}{2}})/2, (y_{k-\frac{1}{2}} + y_{k+\frac{1}{2}})/2)$  with  $x_{j+\frac{1}{2}} - x_{j-\frac{1}{2}} \equiv \Delta x$  and  $y_{k+\frac{1}{2}} - y_{k-\frac{1}{2}} \equiv \Delta y$  for  $j = 1, \dots, N_x$ ,  $k = 1, \dots, N_y$ , and assume that the computed cell averages of  $\mathbf{W}$  over the corresponding cells  $C_{j,k}$ ,

$$\overline{\mathbf{W}}_{j,k}(t) := \frac{1}{\Delta x \Delta y} \int_{C_{j,k}} \mathbf{W}(x, y, t) \, dx dy,$$

103 are available at a certain time level  $t \geq 0$ . Note that  $\overline{\mathbf{W}}_{j,k}$  as well as many of the indexed quantities  
104 introduced below are time-dependent, but from here on, we suppress this dependence for the sake of  
105 brevity.

106 According to [12], the cell averages  $\overline{\mathbf{W}}_{j,k} = (\overline{\mathbf{U}}_{j,k}^\top, \overline{\mathbf{U}}_{j,k}^\top)^\top$  are evolved in time by numerically solving  
107 the following system of ODEs:

$$\begin{aligned} \frac{d\overline{\mathbf{U}}_{j,k}}{dt} &= -\frac{\mathcal{K}_{j+\frac{1}{2},k}^{\text{LCD}} - \mathcal{K}_{j-\frac{1}{2},k}^{\text{LCD}}}{\Delta x} - \frac{\mathcal{L}_{j,k+\frac{1}{2}}^{\text{LCD}} - \mathcal{L}_{j,k-\frac{1}{2}}^{\text{LCD}}}{\Delta y}, \\ \frac{d\overline{\mathbf{U}}_{j,k}}{dt} &= -\frac{\tilde{\mathcal{F}}_{j+\frac{1}{2},k} - \tilde{\mathcal{F}}_{j-\frac{1}{2},k}}{\Delta x} - \frac{\tilde{\mathcal{G}}_{j,k+\frac{1}{2}} - \tilde{\mathcal{G}}_{j,k-\frac{1}{2}}}{\Delta y}, \end{aligned} \quad (3.2)$$

109 where the numerical fluxes  $\tilde{\mathcal{F}}_{j+\frac{1}{2},k}$  and  $\tilde{\mathcal{G}}_{j,k+\frac{1}{2}}$  are evaluated by the CU scheme from [24]

$$\begin{aligned} \tilde{\mathcal{F}}_{j+\frac{1}{2},k} &= \frac{s_{j+\frac{1}{2},k}^+ \tilde{\mathbf{F}}(\mathbf{W}_{j,k}^{\text{E}}) - s_{j+\frac{1}{2},k}^- \tilde{\mathbf{F}}(\mathbf{W}_{j+1,k}^{\text{W}})}{s_{j+\frac{1}{2},k}^+ - s_{j+\frac{1}{2},k}^-} + \frac{s_{j+\frac{1}{2},k}^+ s_{j+\frac{1}{2},k}^-}{s_{j+\frac{1}{2},k}^+ - s_{j+\frac{1}{2},k}^-} (\tilde{\mathbf{U}}_{j+1,k}^{\text{W}} - \tilde{\mathbf{U}}_{j,k}^{\text{E}}), \\ \tilde{\mathcal{G}}_{j,k+\frac{1}{2}} &= \frac{s_{j,k+\frac{1}{2}}^+ \tilde{\mathbf{G}}(\mathbf{W}_{j,k}^{\text{N}}) - s_{j,k+\frac{1}{2}}^- \tilde{\mathbf{G}}(\mathbf{W}_{j,k+1}^{\text{S}})}{s_{j,k+\frac{1}{2}}^+ - s_{j,k+\frac{1}{2}}^-} + \frac{s_{j,k+\frac{1}{2}}^+ s_{j,k+\frac{1}{2}}^-}{s_{j,k+\frac{1}{2}}^+ - s_{j,k+\frac{1}{2}}^-} (\tilde{\mathbf{U}}_{j,k+1}^{\text{S}} - \tilde{\mathbf{U}}_{j,k}^{\text{N}}), \end{aligned} \quad (3.3)$$

111 the global numerical fluxes  $\mathcal{K}_{j+\frac{1}{2},k}^{\text{LCD}}$  and  $\mathcal{L}_{j,k+\frac{1}{2}}^{\text{LCD}}$  are given by

$$\begin{aligned} \mathcal{K}_{j+\frac{1}{2},k}^{\text{LCD}} &= R_{j+\frac{1}{2},k}^x P_{j+\frac{1}{2},k}^{\text{LCD}} (R_{j+\frac{1}{2},k}^x)^{-1} \mathbf{K}_{j,k}^{\text{E}} + R_{j+\frac{1}{2},k}^x M_{j+\frac{1}{2},k}^{\text{LCD}} (R_{j+\frac{1}{2},k}^x)^{-1} \mathbf{K}_{j+1,k}^{\text{W}} \\ &\quad + R_{j+\frac{1}{2},k}^x Q_{j+\frac{1}{2},k}^{\text{LCD}} (R_{j+\frac{1}{2},k}^x)^{-1} (\mathbf{U}_{j+1,k}^{\text{W}} - \mathbf{U}_{j,k}^{\text{E}}), \\ \mathcal{L}_{j,k+\frac{1}{2}}^{\text{LCD}} &= R_{j,k+\frac{1}{2}}^y P_{j,k+\frac{1}{2}}^{\text{LCD}} (R_{j,k+\frac{1}{2}}^y)^{-1} \mathbf{L}_{j,k}^{\text{N}} + R_{j,k+\frac{1}{2}}^y M_{j,k+\frac{1}{2}}^{\text{LCD}} (R_{j,k+\frac{1}{2}}^y)^{-1} \mathbf{L}_{j,k+1}^{\text{S}} \\ &\quad + R_{j,k+\frac{1}{2}}^y Q_{j,k+\frac{1}{2}}^{\text{LCD}} (R_{j,k+\frac{1}{2}}^y)^{-1} (\mathbf{U}_{j,k+1}^{\text{S}} - \mathbf{U}_{j,k}^{\text{N}}), \end{aligned} \quad (3.4)$$

113 and the global fluxes  $\mathbf{K}_{j,k}^{\text{E,W}}$  and  $\mathbf{L}_{j,k}^{\text{N,S}}$  in (3.4) are obtained using (3.1):

$$\mathbf{K}_{j,k}^{\text{E,W}} = \mathbf{F}(\mathbf{U}_{j,k}^{\text{E,W}}) - (\mathbf{I}^x)_{j,k}^{\text{E,W}}, \quad \mathbf{L}_{j,k}^{\text{N,S}} = \mathbf{G}(\mathbf{U}_{j,k}^{\text{N,S}}) - (\mathbf{I}^y)_{j,k}^{\text{N,S}}. \quad (3.5)$$

115 In (3.3)–(3.5), the following quantities have been used.

•  $\mathbf{U}_{j,k}^{\text{E,W,N,S}}$  are the point values of  $\mathbf{U}$  at midpoints of the cell interfaces of  $C_{j,k}$ . They are obtained using a piecewise linear reconstruction applied to the primitive variables  $\mathbf{V}$  using the corresponding LCD. To this end, we first compute

$$\begin{aligned} u_{j,k} &= \frac{(\overline{\rho u})_{j,k}}{\overline{\rho}_{j,k}}, \quad v_{j,k} = \frac{(\overline{\rho v})_{j,k}}{\overline{\rho}_{j,k}}, \quad w_{j,k} = \frac{(\overline{\rho w})_{j,k}}{\overline{\rho}_{j,k}}, \\ p_{j,k} &= (\gamma - 1) \left[ \overline{\mathcal{E}}_{j,k} - \frac{\overline{\rho}_{j,k}}{2} (u_{j,k}^2 + v_{j,k}^2 + w_{j,k}^2) - \frac{1}{2} ((\overline{b_1})_{j,k}^2 + (\overline{b_2})_{j,k}^2 + (\overline{b_3})_{j,k}^2) \right], \end{aligned}$$

116 where the latter expression has been obtained using the EOS (2.2).

We then switch to the local characteristic variables  $\Gamma$  at the midpoints of each of the cell interfaces  $(x_{j+\frac{1}{2}}, y_k)$  and  $(x_j, y_{k+\frac{1}{2}})$ :

$$\begin{aligned}\Gamma_{\ell,k}^x &= (T_{j+\frac{1}{2},k}^x)^{-1} \mathbf{V}_{\ell,k}, \quad \ell = j-1, j, j+1, j+2, \\ \Gamma_{j,m}^y &= (T_{j,k+\frac{1}{2}}^y)^{-1} \mathbf{V}_{j,m}, \quad m = k-1, k, k+1, k+2,\end{aligned}$$

117 where the matrices  $T_{j+\frac{1}{2},k}^x$  and  $T_{j,k+\frac{1}{2}}^y$  are obtained using the LCD for the primitive system (2.10) and  
118 they are given in Appendix B.

119 Next, we perform generalized minmod reconstructions in the  $x$ - and  $y$ -directions to evaluate the slopes  
120

$$\begin{aligned}121 \quad (3.6) \quad (\Gamma_x^x)_{j,k} &= \text{minmod} \left( \theta \frac{\Gamma_{j+1,k}^x - \Gamma_{j,k}^x}{\Delta x}, \frac{\Gamma_{j+1,k}^x - \Gamma_{j-1,k}^x}{2\Delta x}, \theta \frac{\Gamma_{j,k}^x - \Gamma_{j-1,k}^x}{\Delta x} \right), \\ (\Gamma_x^x)_{j+1,k} &= \text{minmod} \left( \theta \frac{\Gamma_{j+2,k}^x - \Gamma_{j+1,k}^x}{\Delta x}, \frac{\Gamma_{j+2,k}^x - \Gamma_{j,k}^x}{2\Delta x}, \theta \frac{\Gamma_{j+1,k}^x - \Gamma_{j,k}^x}{\Delta x} \right),\end{aligned}$$

122 and

$$\begin{aligned}123 \quad (3.7) \quad (\Gamma_y^y)_{j,k} &= \text{minmod} \left( \theta \frac{\Gamma_{j,k+1}^y - \Gamma_{j,k}^y}{\Delta y}, \frac{\Gamma_{j,k+1}^y - \Gamma_{j,k-1}^y}{2\Delta y}, \theta \frac{\Gamma_{j,k}^y - \Gamma_{j,k-1}^y}{\Delta y} \right), \\ (\Gamma_y^y)_{j,k+1} &= \text{minmod} \left( \theta \frac{\Gamma_{j,k+2}^y - \Gamma_{j,k+1}^y}{\Delta y}, \frac{\Gamma_{j,k+2}^y - \Gamma_{j,k}^y}{2\Delta y}, \theta \frac{\Gamma_{j,k+1}^y - \Gamma_{j,k}^y}{\Delta y} \right),\end{aligned}$$

respectively. In (3.6) and (3.7), the minmod function is defined as

$$\text{minmod}(z_1, z_2, \dots) := \begin{cases} \min_j \{z_j\} & \text{if } z_j > 0 \quad \forall j, \\ \max_j \{z_j\} & \text{if } z_j < 0 \quad \forall j, \\ 0 & \text{otherwise,} \end{cases}$$

124 and it is applied in a component-wise manner. The parameter  $\theta \in [1, 2]$  is used to control the non-  
125 oscillatory property of the resulting scheme: larger  $\theta$  typically leads to a sharper, but more oscillatory  
126 computed solution.

We then evaluate the corresponding one-sided point values:

$$\begin{aligned}(\Gamma_{j,k}^x)^E &= \Gamma_{j,k}^x + \frac{\Delta x}{2} (\Gamma_x^x)_{j,k}, & (\Gamma_{j+1,k}^x)^W &= \Gamma_{j+1,k}^x - \frac{\Delta x}{2} (\Gamma_x^x)_{j+1,k}, \\ (\Gamma_{j,k}^y)^N &= \Gamma_{j,k}^y + \frac{\Delta y}{2} (\Gamma_y^y)_{j,k}, & (\Gamma_{j,k+1}^y)^S &= \Gamma_{j,k+1}^y - \frac{\Delta y}{2} (\Gamma_y^y)_{j,k+1},\end{aligned}$$

127 switch back to the primitive variables:

$$128 \quad \mathbf{V}_{j,k}^E = T_{j+\frac{1}{2},k}^x (\Gamma_{j,k}^x)^E, \quad \mathbf{V}_{j+1,k}^W = T_{j+\frac{1}{2},k}^x (\Gamma_{j+1,k}^x)^W, \quad \mathbf{V}_{j,k}^N = T_{j,k+\frac{1}{2}}^y (\Gamma_{j,k}^y)^N, \quad \mathbf{V}_{j,k+1}^S = T_{j,k+\frac{1}{2}}^y (\Gamma_{j,k+1}^y)^S,$$

129 and then transform  $\mathbf{V}_{j,k}^{E,W,N,S}$  into  $\mathbf{U}_{j,k}^{E,W,N,S}$ , which are non-oscillatory, but they do not necessarily satisfy  
130 the local divergence-free requirement, which can be written as

$$131 \quad (3.8) \quad (\nabla \cdot \mathbf{b})_{j,k} := \frac{(b_1)_{j,k}^E - (b_1)_{j,k}^W}{\Delta x} + \frac{(b_2)_{j,k}^N - (b_2)_{j,k}^S}{\Delta y} \equiv 0, \quad \forall j, k.$$

132 We thus need to correct the point values  $(b_1)_{j,k}^{E,W}$  and  $(b_2)_{j,k}^{N,S}$ . To this end, we proceed similarly  
133 to [9, §2.2.1] by setting the slopes

$$134 \quad (3.9) \quad ((b_1)_x)_{j,k} = \sigma_{j,k} \bar{A}_{j,k} \quad \text{and} \quad ((b_2)_y)_{j,k} = \sigma_{j,k} \bar{B}_{j,k},$$

135 where

$$136 \quad (3.10) \quad \sigma_{j,k} = \min \{1, \sigma_{j,k}^x, \sigma_{j,k}^y\},$$

137 and the scaling factors  $\sigma_{j,k}^x$  and  $\sigma_{j,k}^y$  are computed by

$$138 \quad (3.11) \quad \sigma_{j,k}^x := \begin{cases} \min \{1, \sigma_{j,k}^{x,1}, \sigma_{j,k}^{x,2}\} & \text{if } \sigma_{j,k}^{x,1} > 0, \sigma_{j,k}^{x,2} > 0, \text{ and } \bar{A}_{j,k} \neq 0 \\ 0 & \text{otherwise} \end{cases}$$

139 and

$$140 \quad (3.12) \quad \sigma_{j,k}^y := \begin{cases} \min \{1, \sigma_{j,k}^{y,1}, \sigma_{j,k}^{y,2}\} & \text{if } \sigma_{j,k}^{y,1} > 0, \sigma_{j,k}^{y,2} > 0, \text{ and } \bar{B}_{j,k} \neq 0 \\ 0 & \text{otherwise,} \end{cases}$$

141 where

$$142 \quad (3.13) \quad \begin{aligned} \sigma_{j,k}^{x,1} &= \frac{2((\hat{b}_1)_{j,k}^E - (\bar{b}_1)_{j,k})}{\Delta x \bar{A}_{j,k}}, & \sigma_{j,k}^{x,2} &= \frac{2((\bar{b}_1)_{j,k} - (\hat{b}_1)_{j,k}^W)}{\Delta x \bar{A}_{j,k}}, \\ \sigma_{j,k}^{y,1} &= \frac{2((\hat{b}_2)_{j,k}^N - (\bar{b}_2)_{j,k})}{\Delta y \bar{B}_{j,k}}, & \sigma_{j,k}^{y,2} &= \frac{2((\bar{b}_2)_{j,k} - (\hat{b}_2)_{j,k}^S)}{\Delta y \bar{B}_{j,k}}, \end{aligned}$$

143 and  $(\hat{b}_1)_{j,k}^{E,W}$  and  $(\hat{b}_2)_{j,k}^{N,S}$  denote the point values of  $b_1$  and  $b_2$ , which have been reconstructed as described  
144 above. We then correct the corresponding one-sided point values:

$$145 \quad (3.14) \quad \begin{aligned} ((b_1)_{j,k})^E &= (\bar{b}_1)_{j,k} + \frac{\Delta x}{2} ((b_1)_x)_{j,k}, & ((b_1)_{j+1,k})^W &= (\bar{b}_1)_{j+1,k} - \frac{\Delta x}{2} ((b_1)_x)_{j+1,k}, \\ ((b_2)_{j,k})^N &= (\bar{b}_2)_{j,k} + \frac{\Delta y}{2} ((b_2)_y)_{j,k}, & ((b_2)_{j,k+1})^S &= (\bar{b}_2)_{j,k+1} - \frac{\Delta y}{2} ((b_2)_y)_{j,k+1}. \end{aligned}$$

146 • The one-sided point values  $\tilde{U}_{j,k}^{E,W,N,S}$  are obtained by applying the generalized minmod reconstruction  
147 directly to the  $A$  and  $B$  fields.

148 • The point values of the global variables  $\mathbf{I}^x$  and  $\mathbf{I}^y$  in (3.5) are computed recursively. We first set  $\hat{x} = x_{\frac{1}{2}}$   
149 and  $\hat{y} = y_{\frac{1}{2}}$  so that  $(\mathbf{I}^x)_{\frac{1}{2},k}^- := \mathbf{0}$  and  $(\mathbf{I}^y)_{j,\frac{1}{2}}^- := \mathbf{0}$ , and then evaluate  $(\mathbf{I}^x)_{\frac{1}{2},k}^+ = \mathbf{Q}_{\Psi,\frac{1}{2},k}^x$ ,  $(\mathbf{I}^y)_{j,\frac{1}{2}}^+ = \mathbf{Q}_{\Psi,j,\frac{1}{2}}^y$ ,  
150 and

$$151 \quad \begin{aligned} (\mathbf{I}^x)_{j+\frac{1}{2},k}^- &= (\mathbf{I}^x)_{j-\frac{1}{2},k}^+ + \mathbf{Q}_{j,k}^x, & (\mathbf{I}^x)_{j+\frac{1}{2},k}^+ &= (\mathbf{I}^x)_{j+\frac{1}{2},k}^- + \mathbf{Q}_{\Psi,j+\frac{1}{2},k}^x, \\ (\mathbf{I}^y)_{j,k+\frac{1}{2}}^- &= (\mathbf{I}^y)_{j,k-\frac{1}{2}}^+ + \mathbf{Q}_{j,k}^y, & (\mathbf{I}^y)_{j,k+\frac{1}{2}}^+ &= (\mathbf{I}^y)_{j,k+\frac{1}{2}}^- + \mathbf{Q}_{\Psi,j,k+\frac{1}{2}}^y, \end{aligned}$$

152 for  $j = 1, \dots, N_x$ ,  $k = 1, \dots, N_y$ . Here,  $\mathbf{Q}_{j,k}^x$ ,  $\mathbf{Q}_{\Psi,j+\frac{1}{2},k}^x$ ,  $\mathbf{Q}_{j,k}^y$ , and  $\mathbf{Q}_{\Psi,j,k+\frac{1}{2}}^y$  are the terms reflecting the  
153 contribution of the nonconservative terms  $Q^x(\mathbf{U})\mathbf{U}_x$  and  $Q^y(\mathbf{U})\mathbf{U}_y$ . For the details on evaluating these  
154 terms, we refer the readers to [9, §2.2.3].

•  $P_{j+\frac{1}{2},k}^{\text{LCD}}$ ,  $M_{j+\frac{1}{2},k}^{\text{LCD}}$ ,  $Q_{j+\frac{1}{2},k}^{\text{LCD}}$ ,  $P_{j,k+\frac{1}{2}}^{\text{LCD}}$ ,  $M_{j,k+\frac{1}{2}}^{\text{LCD}}$ , and  $Q_{j,k+\frac{1}{2}}^{\text{LCD}}$  in (3.4) are diagonal matrices

$$\begin{aligned} P_{j+\frac{1}{2},k}^{\text{LCD}} &= \text{diag} \left( (P_1^{\text{LCD}})_{j+\frac{1}{2},k}, \dots, (P_8^{\text{LCD}})_{j+\frac{1}{2},k} \right), & P_{j,k+\frac{1}{2}}^{\text{LCD}} &= \text{diag} \left( (P_1^{\text{LCD}})_{j,k+\frac{1}{2}}, \dots, (P_8^{\text{LCD}})_{j,k+\frac{1}{2}} \right), \\ M_{j+\frac{1}{2},k}^{\text{LCD}} &= \text{diag} \left( (M_1^{\text{LCD}})_{j+\frac{1}{2},k}, \dots, (M_8^{\text{LCD}})_{j+\frac{1}{2},k} \right), & M_{j,k+\frac{1}{2}}^{\text{LCD}} &= \text{diag} \left( (M_1^{\text{LCD}})_{j,k+\frac{1}{2}}, \dots, (M_8^{\text{LCD}})_{j,k+\frac{1}{2}} \right), \\ Q_{j+\frac{1}{2},k}^{\text{LCD}} &= \text{diag} \left( (Q_1^{\text{LCD}})_{j+\frac{1}{2},k}, \dots, (Q_8^{\text{LCD}})_{j+\frac{1}{2},k} \right), & Q_{j,k+\frac{1}{2}}^{\text{LCD}} &= \text{diag} \left( (Q_1^{\text{LCD}})_{j,k+\frac{1}{2}}, \dots, (Q_8^{\text{LCD}})_{j,k+\frac{1}{2}} \right), \end{aligned}$$

where

$$\begin{aligned} ((P_i^{\text{LCD}})_{j+\frac{1}{2},k}, (M_i^{\text{LCD}})_{j+\frac{1}{2},k}, (Q_i^{\text{LCD}})_{j+\frac{1}{2},k}) &= \frac{\left( (\lambda_i^+)_{j+\frac{1}{2},k}, -(\lambda_i^-)_{j+\frac{1}{2},k}, (\lambda_i^+)_{j+\frac{1}{2},k} (\lambda_i^-)_{j+\frac{1}{2},k} \right)}{(\lambda_i^+)_{j+\frac{1}{2},k} - (\lambda_i^-)_{j+\frac{1}{2},k}}, \\ ((P_i^{\text{LCD}})_{j,k+\frac{1}{2}}, (M_i^{\text{LCD}})_{j,k+\frac{1}{2}}, (Q_i^{\text{LCD}})_{j,k+\frac{1}{2}}) &= \frac{\left( (\lambda_i^+)_{j,k+\frac{1}{2}}, -(\lambda_i^-)_{j,k+\frac{1}{2}}, (\lambda_i^+)_{j,k+\frac{1}{2}} (\lambda_i^-)_{j,k+\frac{1}{2}} \right)}{(\lambda_i^+)_{j,k+\frac{1}{2}} - (\lambda_i^-)_{j,k+\frac{1}{2}}}, \end{aligned}$$

155 with

$$\begin{aligned}
 & (\lambda_i^+)_{j+\frac{1}{2},k} = \max \{ \lambda_i(C^x(\mathbf{U}_{j,k}^E)), \lambda_i(C^x(\mathbf{U}_{j+1,k}^W)), \varepsilon \}, \\
 & (\lambda_i^-)_{j+\frac{1}{2},k} = \min \{ \lambda_i(C^x(\mathbf{U}_{j,k}^E)), \lambda_i(C^x(\mathbf{U}_{j+1,k}^W)), -\varepsilon \}, \\
 & (\lambda_i^+)_{j,k+\frac{1}{2}} = \max \{ \lambda_i(C^y(\mathbf{U}_{j,k}^N)), \lambda_i(C^y(\mathbf{U}_{j,k+1}^S)), \varepsilon \}, \\
 & (\lambda_i^-)_{j,k+\frac{1}{2}} = \min \{ \lambda_i(C^y(\mathbf{U}_{j,k}^N)), \lambda_i(C^y(\mathbf{U}_{j,k+1}^S)), -\varepsilon \},
 \end{aligned}
 \tag{3.15}$$

157 and  $\lambda_i(C^x(\mathbf{U}))$  and  $\lambda_i(C^y(\mathbf{U}))$  are eigenvalues of  $C^x$  and  $C^y$ ,  $i = 1, \dots, 8$ , respectively; see Appendix  
 158 A for details. In (3.15),  $\varepsilon$  is a small desingularization constant, which is taken to be  $10^{-8}$  in all of the  
 159 numerical examples reported in §4.

160 •  $R_{j+\frac{1}{2},k}^x$  and  $R_{j,k+\frac{1}{2}}^y$  are the matrices of right eigenvectors of  $\widehat{C}_{j+\frac{1}{2},k}^x = C^x(\widehat{\mathbf{U}}_{j+\frac{1}{2},k})$  and  $\widehat{C}_{j,k+\frac{1}{2}}^y =$   
 161  $C^y(\widehat{\mathbf{U}}_{j,k+\frac{1}{2}})$ , respectively. Here, we take  $\widehat{\mathbf{U}}_{j+\frac{1}{2},k} = (\overline{\mathbf{U}}_{j,k} + \overline{\mathbf{U}}_{j+1,k})/2$  and  $\widehat{\mathbf{U}}_{j,k+\frac{1}{2}} = (\overline{\mathbf{U}}_{j,k} + \overline{\mathbf{U}}_{j,k+1})/2$ .

162 •  $s_{j+\frac{1}{2},k}^\pm$  and  $s_{j,k+\frac{1}{2}}^\pm$  are one-sided local speeds of propagation in the  $x$ - and  $y$ -direction, respectively. They  
 163 are estimated as in [9, §2.2.2].

164 *Remark 3.1.* We stress that the correction of the point values (3.9)–(3.14) together with the result  
 165 proven in [9, Theorem 2.2] enforce the local divergence-free condition (3.8).

166 **4. Numerical Examples.** In this section, we test the developed LCD-PCCU scheme on a number  
 167 of numerical examples and compare the obtained results with those computed by the PCCU scheme  
 168 from [9]. We numerically integrate the ODE systems (3.2) by the three-stage third-order strong stability  
 169 preserving (SSP) Runge-Kutta method (see, e.g., [21, 22]), use the CFL number 0.25, and set the minmod  
 170 parameter  $\theta = 1.3$  (except for Example 5, where we take  $\theta = 1$  to reduce oscillations). The specific heat  
 171 ratio  $\gamma$  is either 2 (Example 1),  $5/3$  (Examples 2–4), or 1.4 (Example 5).

172 In Examples 2 and 3, we will demonstrate how the discrete divergence  $(\nabla \cdot \mathbf{b})_{j,k}$ , defined in (3.8),  
 173 increases in time if the correction (3.9)–(3.13) of the slopes  $((b_1)_x)_{j,k}$  and  $((b_2)_y)_{j,k}$  is not implemented  
 174 (the corresponding scheme will be referred to as Uncorrected LCD-PCCU scheme).

175 **Example 1—Brio-Wu Shock-Tube Problem.** In the first example taken from [5], we consider  
 176 the one-dimensional (1-D) Riemann problem, which is a benchmark widely used to test the ability of  
 177 schemes to capture compound waves that emerge out of the initial data,

$$(\rho, u, v, w, b_1, b_2, b_3, p)(x, 0) = \begin{cases} (1, 0, 0, 0, 0.75, 1, 0, 1) & \text{if } x < 0, \\ (0.125, 0, 0, 0, 0.75, -1, 0, 0.1) & \text{otherwise,} \end{cases}$$

179 which depend on  $x$  only. We conduct a 2-D computation on the domain  $[-1, 1] \times [-0.01, 0.01]$  subject to  
 180 the free boundary conditions.

181 We compute the solutions by the LCD-PCCU and PCCU schemes until the final time  $t = 0.2$  on a  
 182 uniform mesh consisting of  $200 \times 2$  cells. The cross-sectional profiles at  $y = 0$  of  $\rho$ ,  $b_1$ , and  $b_2$  are presented  
 183 in Figure 4.1 along with the reference solution computed by the PCCU scheme on a significantly finer mesh  
 184 of  $10000 \times 2$  cells. One can observe that the solution consists of several nonsmooth structures, including  
 185 rarefaction waves, shock waves traveling at various speeds, a contact discontinuity, and a compound shock  
 186 wave. Both the LCD-PCCU and PCCU schemes successfully capture all of these complex structures.  
 187 However, the numerical results obtained by the LCD-PCCU scheme exhibit somewhat higher resolution  
 188 compared to those produced by the PCCU scheme.

**Example 2—Circularly Polarized Alfvén Wave.** In the second example taken from [36], we  
 consider the time evolution of a circularly polarized Alfvén wave that travels at a constant speed at an  
 angle of  $\alpha = \pi/6$  with respect to the  $x$ -axis. In this example, designed to check the experimental order of  
 accuracy of the studied schemes, the initial conditions are

$$\begin{aligned}
 \rho(x, y, 0) &\equiv 1, & u(x, y, 0) &= v_{\parallel} \cos \alpha + v_{\perp} \sin \alpha, & v(x, y, 0) &= v_{\parallel} \sin \alpha - v_{\perp} \cos \alpha, \\
 p(x, y, 0) &\equiv 0.1, & b_1(x, y, 0) &= b_{\parallel} \cos \alpha + b_{\perp} \sin \alpha, & b_2(x, y, 0) &= b_{\parallel} \sin \alpha - b_{\perp} \cos \alpha, \\
 w(x, y, 0) &= b_3(x, y, 0) = 0.1 \cos [2\pi(x \cos \alpha + y \sin \alpha)],
 \end{aligned}$$

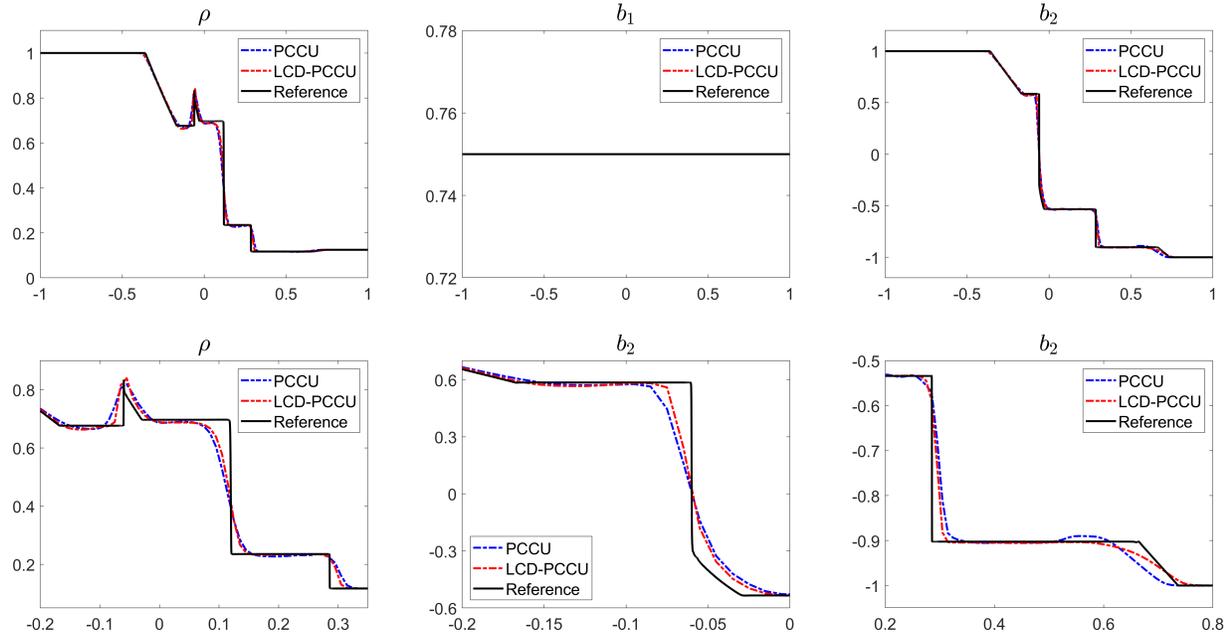


FIG. 4.1. Example 1:  $\rho$ ,  $b_1$ , and  $b_2$  computed by the LCD-PCCU and PCCU schemes (top row) and zooms for  $\rho$  and  $b_2$  at  $x \in [-0.2, 0.35]$ ,  $[-0.2, 0]$ , and  $[0.2, 0.8]$  (bottom row).

where

$$v_{\parallel} = 0, \quad b_{\parallel} = 1, \quad v_{\perp} = b_{\perp} = 0.1 \sin [2\pi(x \cos \alpha + y \sin \alpha)],$$

189 and the periodic boundary conditions are imposed in the computational domain  $[0, \frac{1}{\cos \alpha}] \times [0, \frac{1}{\sin \alpha}]$ . It is  
 190 easy to show that the solution of the resulting initial-boundary value problem is a traveling wave, which  
 191 returns to its initial position at any integer time  $t$ .

192 We compute the solutions by the LCD-PCCU and PCCU schemes until the final time  $t = 5$  on a  
 193 sequence of uniform meshes with  $20 \times 20$ ,  $40 \times 40$ ,  $80 \times 80$ ,  $160 \times 160$ , and  $320 \times 320$  cells, and compute  
 194 the  $L^1$ -norm of the differences between the numerical and exact solutions. We report the  $L^1$ -errors  
 195 and corresponding experimental rates of convergence for both  $u$  and  $b_3$  in Table 4.1, where one can see  
 196 that while both the LCD-PCCU and PCCU schemes achieve the expected second order of accuracy, the  
 magnitudes of the errors are slightly smaller for the proposed LCD-PCCU scheme.

TABLE 4.1

Example 2:  $L^1$ -errors and experimental convergence rates for  $u$  and  $b_3$  computed by the LCD-PCCU and PCCU schemes.

Mesh	LCD-PCCU Scheme				PCCU Scheme			
	$u$		$b_3$		$u$		$b_3$	
	Error	Rate	Error	Rate	Error	Rate	Error	Rate
$20 \times 20$	2.69e-2	–	4.50e-2	–	3.38e-2	–	6.45e-2	–
$40 \times 40$	7.83e-3	1.78	1.18e-2	1.93	7.98e-3	2.08	1.67e-2	1.95
$80 \times 80$	2.29e-3	1.78	3.29e-3	1.84	2.46e-3	1.70	5.32e-3	1.65
$160 \times 160$	5.75e-4	1.99	8.31e-4	1.98	6.48e-4	1.93	1.41e-3	1.92
$320 \times 320$	1.34e-4	2.10	2.19e-4	1.93	1.54e-4	2.08	3.34e-4	2.07

197

198 Figure 4.2 presents the time evolution of the  $L^1$ - and  $L^\infty$ -norms of  $(\nabla \cdot \mathbf{b})_{j,k}$  computed by the  
 199 Uncorrected LCD-PCCU scheme on a uniform  $320 \times 320$  mesh. As one can see, the magnitudes of both  
 200 norms are comparable or even exceed the size of the formal truncation error, which is about  $10^{-5}$  on  
 201 this grid. This suggests that the use of the Uncorrected LCD-PCCU scheme may lead to a substantial

202 numerical inaccuracy, and thus applying the divergence-free correction might be essential for ensuring the  
 203 physical consistency and long-term stability of the simulation.

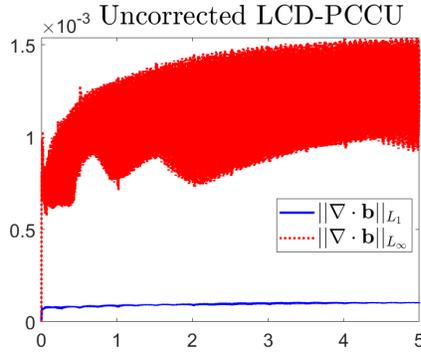


FIG. 4.2. Example 2: Time evolution of the  $L^1$ - and  $L^\infty$ -norms of  $(\nabla \cdot \mathbf{b})_{j,k}$  computed by the Uncorrected LCD-PCCU scheme on a uniform  $320 \times 320$  mesh.

203

**Example 3—Orszag-Tang Vortex Problem.** In this example taken from [30], we consider the Orszag-Tang vortex problem, which has been widely used as a benchmark due to the formation and interaction of multiple shocks as the system evolves in time and to the presence of many important features of MHD turbulence. The initial conditions,

$$\begin{aligned} \rho(x, y, 0) &\equiv \gamma^2, & u(x, y, 0) &= -\sin y, & v(x, y, 0) &= \sin x, & w(x, y, 0) &\equiv 0, \\ b_1(x, y, 0) &= -\sin y, & b_2(x, y, 0) &= \sin(2x), & b_3(x, y, 0) &\equiv 0, & p(x, y, 0) &\equiv \gamma, \end{aligned}$$

204 are prescribed in the computational domain  $[0, 2\pi] \times [0, 2\pi]$  subject to the periodic boundary conditions.

205 We compute the numerical solutions by both the LCD-PCCU and PCCU schemes until the final time  
 206  $t = 4$  using a uniform  $200 \times 200$  mesh and plot the obtained densities in Figure 4.3. As one can see, the  
 207 LCD-PCCU solution is sharper, and this can be further seen in Figure 4.4, where we plot the 1-D slices  
 208 of both densities along  $y = \pi$  together with the reference solution computed by the PCCU scheme on  
 $1000 \times 1000$  uniform mesh.

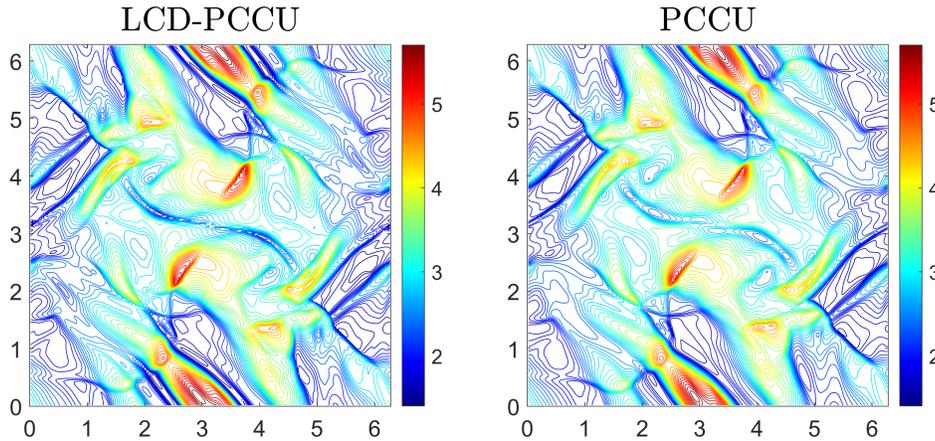


FIG. 4.3. Example 3: Density  $\rho$  computed by the LCD-PCCU (left) and PCCU (right) schemes.

209

210 The time evolution of the  $L^1$ - and  $L^\infty$ -norms of  $(\nabla \cdot \mathbf{b})_{j,k}$  computed by the Uncorrected LCD-PCCU  
 211 scheme is presented in Figure 4.5. As one can see, the magnitudes of both norms increase in time and  
 212 in this example, they are several orders of magnitude larger than the formal truncation error, which is  
 213 about  $10^{-3}$  on this grid. Consequently, applying the divergence-free correction is essential for ensuring  
 214 the physical consistency and long-term stability of the simulation.

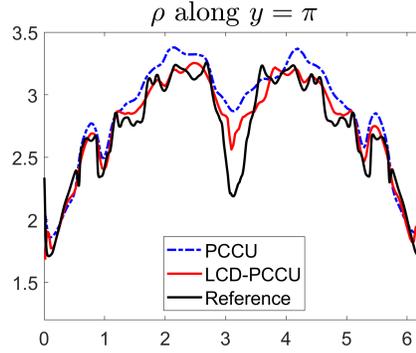


FIG. 4.4. Example 3: 1-D slices along the line  $y = \pi$  of the solutions from Figure 4.3 together with the reference solution.

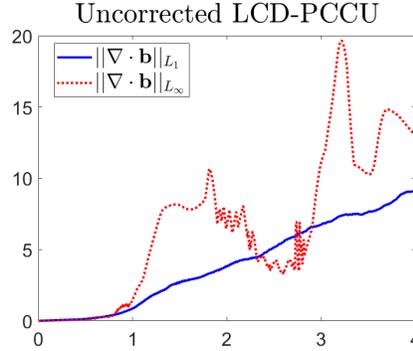


FIG. 4.5. Example 3: Time evolution of the  $L^1$ - and  $L^\infty$ -norms of  $(\nabla \cdot \mathbf{b})_{j,k}$  computed by the Uncorrected LCD-PCCU scheme.

215 **Example 4—Rotor Problem.** In this example, we study the “second rotor problem”, originally  
 216 introduced in [3,36] as a benchmark featuring a rapidly rotating, dense fluid disk embedded in a stationary  
 217 background. As time progresses, the disk undergoes both expansion and rotation.

218 The initial conditions are

$$\begin{aligned}
 219 \quad (\rho, u, v) \Big|_{(x,y,0)} &= \begin{cases} \left( 10, \frac{0.5-y}{r_0}, \frac{x-0.5}{r_0} \right), & r < 0.1, \\ \left( 1 + 9\mu, \frac{\mu(0.5-y)}{r}, \frac{\mu(x-0.5)}{r} \right), & 0.1 \leq r \leq 0.115, \\ (1, 0, 0), & r > 0.115, \end{cases} \\
 220 \quad w(x, y, 0) = b_2(x, y, 0) = b_3(x, y, 0) &\equiv 0, \quad b_1(x, y, 0) \equiv \frac{2.5}{\sqrt{4\pi}}, \quad p(x, y, 0) \equiv 0.5,
 \end{aligned}$$

220 where  $r = \sqrt{(x-0.5)^2 + (y-0.5)^2}$ ,  $r_0 = 0.1$ , and  $\mu = (0.115 - r)/0.015$ . We use the periodic boundary  
 221 conditions in the computational domain  $[0, 1] \times [0, 1]$ .

222 We compute the numerical solutions by both the LCD-PCCU and PCCU schemes until the final time  
 223  $t = 0.295$  using a uniform  $200 \times 200$  mesh and plot the obtained  $\rho$  and  $p$  in Figure 4.6, where one can see  
 224 that the LCD-PCCU scheme achieves higher resolution. To further demonstrate this, we show (in Figure  
 225 4.7) the 1-D slices of both densities along  $x = 0.3$  together with the reference solution computed by the  
 226 PCCU scheme on  $1000 \times 1000$  uniform mesh.

227 **Example 5—Blast Problem.** In the last example taken from [3], we consider the blast problem,  
 228 which poses a significant challenge due to the low gas pressure and presence of strong magnetosonic shocks,  
 229 which frequently lead to the occurrence of negative pressures near the shocks; see [26,27] and references  
 230 therein.

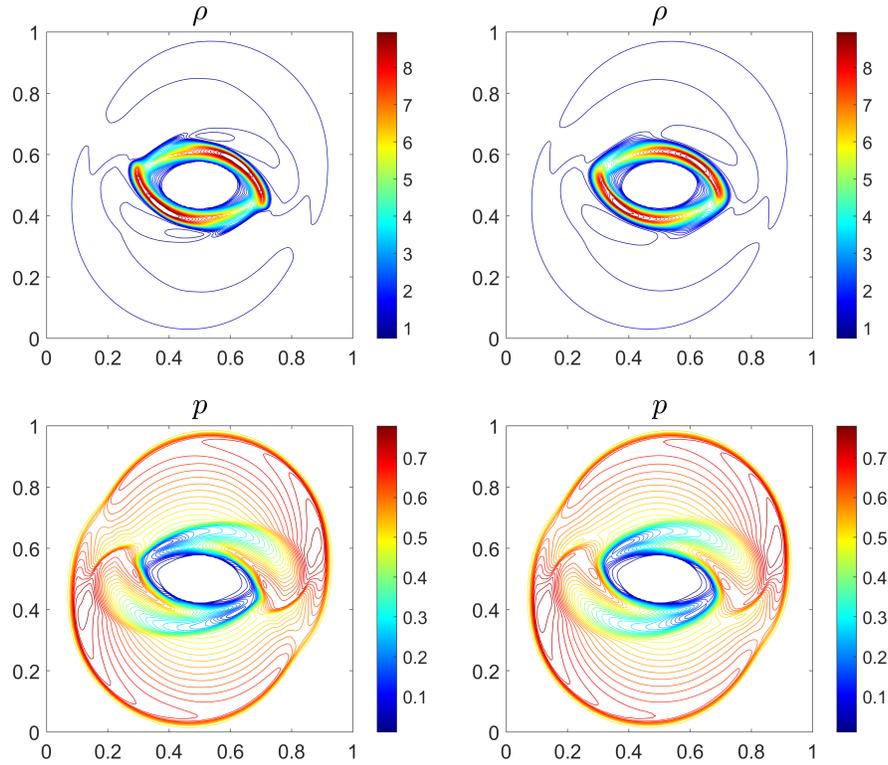


FIG. 4.6. Example 4: Density  $\rho$  (top row) and pressure  $p$  (bottom row) computed by the LCD-PCCU (left column) and PCCU (right column) schemes.

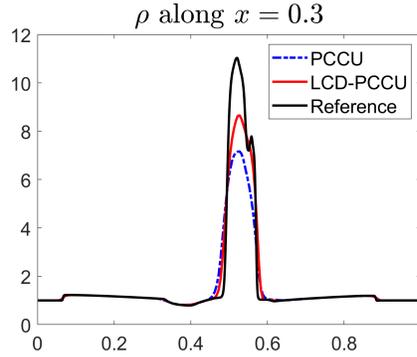


FIG. 4.7. Example 4: 1-D slices along the line  $x = 0.3$  of the densities from Figure 4.6 together with the reference solution.

The initial conditions,

$$(\rho, u, v, w, b_1, b_2, b_3) \Big|_{(x,y,0)} = \left( 1, 0, 0, 0, \frac{50}{\sqrt{\pi}}, 0, 0 \right), \quad p(x, y, 0) = \begin{cases} 1000, & \sqrt{x^2 + y^2} < 0.1, \\ 0.1 & \text{otherwise,} \end{cases}$$

231 are prescribed in the computational domain  $[-0.5, 0.5] \times [-0.5, 0.5]$  subject to the zero-order extrapolation  
 232 imposed at the boundary.

233 We compute the numerical solutions by both the LCD-PCCU and PCCU schemes until the final time  
 234  $t = 0.01$  on a uniform  $200 \times 200$  mesh and plot the obtained density  $\rho$ , pressure  $p$ , velocity magnitude  
 235  $|\mathbf{u}|$ , and magnetic pressure  $|\mathbf{b}|^2/2$  in Figure 4.8. As one can see, the numerical results computed by the  
 236 LCD-PCCU scheme are visibly sharper. However, they contain wiggles in the areas of high density and  
 237 pressure. To experimentally verify that these structures are not numerical artifacts, we refine the mesh  
 238 and perform the same computations on a uniform  $1000 \times 1000$  mesh. The obtained results reported in the

239 left two columns of Figure 4.9, indicate that similar structures start developing in the PCCU solution as  
 240 well. We thus further refine the mesh and run the PCCU simulation on an even finer  $2000 \times 2000$  mesh;  
 241 see Figure 4.9 (right column). One can observe that those wiggly structures are now clearly present in the  
 242 PCCU results. One can notice that the resolution achieved by the LCD-PCCU scheme on the  $1000 \times 1000$   
 243 mesh is practically the same as that achieved by the PCCU scheme on the  $2000 \times 2000$  mesh. This clearly  
 244 indicates an advantage of the proposed LCD-PCCU scheme.

245 **5. Conclusions.** In this paper, we have developed a locally divergence-free local characteristic de-  
 246 composition (LCD) based path-conservative central-upwind (LCD-PCCU) scheme for the ideal magne-  
 247 tohydrodynamics (MHD) equations. The proposed scheme is applied to the Godunov-Powell noncon-  
 248 servative modifications of the studied MHD systems, which have a complete eigenstructure required to  
 249 derive LCD-based central-upwind numerical fluxes; see [8, 12]. In order to ensure the local divergence-free  
 250 property, we have followed [9] and augmented the studied systems with the evolution equations for the  
 251 corresponding derivatives of the magnetic field components and by using these evolved quantities in the  
 252 design of a special piecewise linear reconstruction of the magnetic field, which also guarantees a non-  
 253 oscillatory nature of the resulting scheme. The designed LCD-PCCU scheme has been tested on several  
 254 benchmarks, and the obtained numerical results demonstrate that the proposed scheme outperforms its  
 255 PCCU counterpart from [9].

256 **Appendix A. Eigendecomposition for Conservative Variables.** In this appendix, we provide  
 257 the reader with the matrices used in the LCD of the quasi-linear system (2.9); see [5] for details.

258 First, the matrices  $C^x$  and  $C^y$  are

$$259 \quad (A.1) \quad C^x(\mathbf{U}) = \begin{pmatrix} 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ a_1 & \gamma_3 u_N & \gamma_1 u_T & \gamma_1 w & -\gamma_1 & b_1 & \gamma_2 b_2 & \gamma_2 b_3 \\ -u_N u_T & u_T & u_N & 0 & 0 & b_2 & -b_N & 0 \\ -u_N w & w & 0 & u_N & 0 & b_3 & 0 & -b_N \\ a_2 & a_3 & a_4 & a_5 & \gamma u_N & \mathbf{u} \cdot \mathbf{b} & a_6 & a_7 \\ 0 & 0 & 0 & 0 & 0 & u & 0 & 0 \\ \frac{u_T b_N - u_N b_T}{\rho} & \frac{b_T}{\rho} & -\frac{b_N}{\rho} & 0 & 0 & v & u_N & 0 \\ \frac{w b_N - u_N b_3}{\rho} & \frac{b_3}{\rho} & 0 & -\frac{b_N}{\rho} & 0 & w & 0 & u_N \end{pmatrix},$$

260 and

$$261 \quad (A.2) \quad C^y(\mathbf{U}) = \begin{pmatrix} 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ -u_N u_T & u_N & u_T & 0 & 0 & -b_N & b_1 & 0 \\ a_1 & \gamma_1 u_T & \gamma_3 u_N & \gamma_1 w & -\gamma_1 & \gamma_2 b_2 & b_2 & \gamma_2 b_3 \\ -u_N w & 0 & w & u_N & 0 & 0 & b_3 & -b_N \\ a_2 & a_4 & a_3 & a_5 & \gamma u_N & a_6 & \mathbf{u} \cdot \mathbf{b} & a_7 \\ \frac{u_T b_N - u_N b_T}{\rho} & -\frac{b_N}{\rho} & \frac{b_T}{\rho} & 0 & 0 & u_N & u & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & v & 0 \\ \frac{w b_N - u_N b_3}{\rho} & 0 & \frac{b_3}{\rho} & -\frac{b_N}{\rho} & 0 & 0 & w & u_N \end{pmatrix},$$

where  $u_N$ ,  $b_N$  and  $u_T$ ,  $b_T$  are the normal and tangential components of  $\mathbf{u}$  and  $\mathbf{b}$  with respect to the  $x$ - and  $y$ -axis, namely,

$$(u_N, u_T, b_N, b_T) := \begin{cases} (u, v, b_1, b_2) & \text{in the } x\text{-direction (in (A.1))}, \\ (v, u, b_2, b_1) & \text{in the } y\text{-direction (in (A.2))}, \end{cases}$$

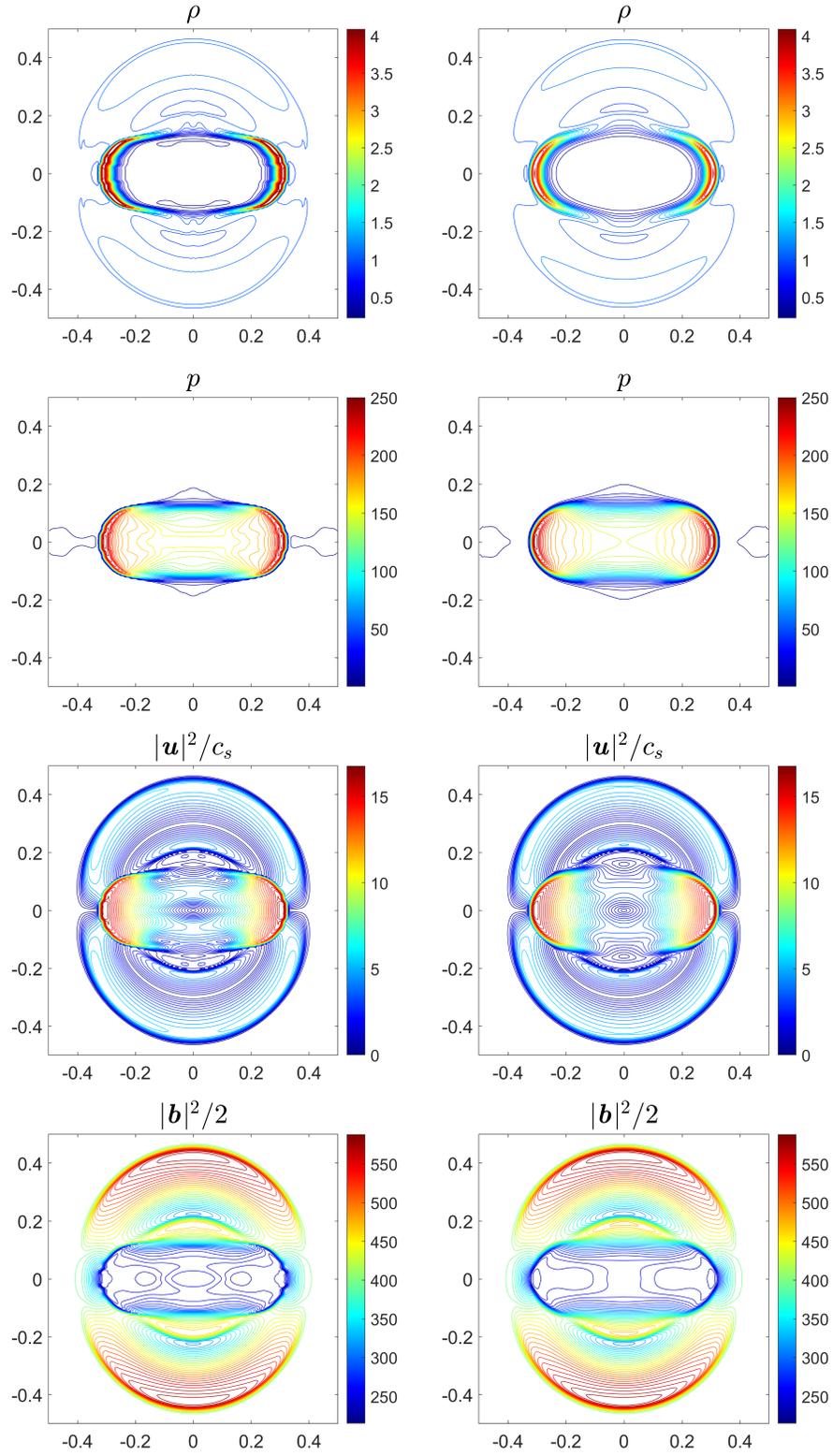


FIG. 4.8. Example 5: Density  $\rho$  (top row), pressure  $p$  (second row), velocity magnitude  $|\mathbf{u}|$  (third row), and magnetic pressure  $|\mathbf{b}|^2/2$  (bottom row) computed by the LCD-PCCU (left column) and PCCU (right column) schemes on a uniform  $200 \times 200$  mesh.

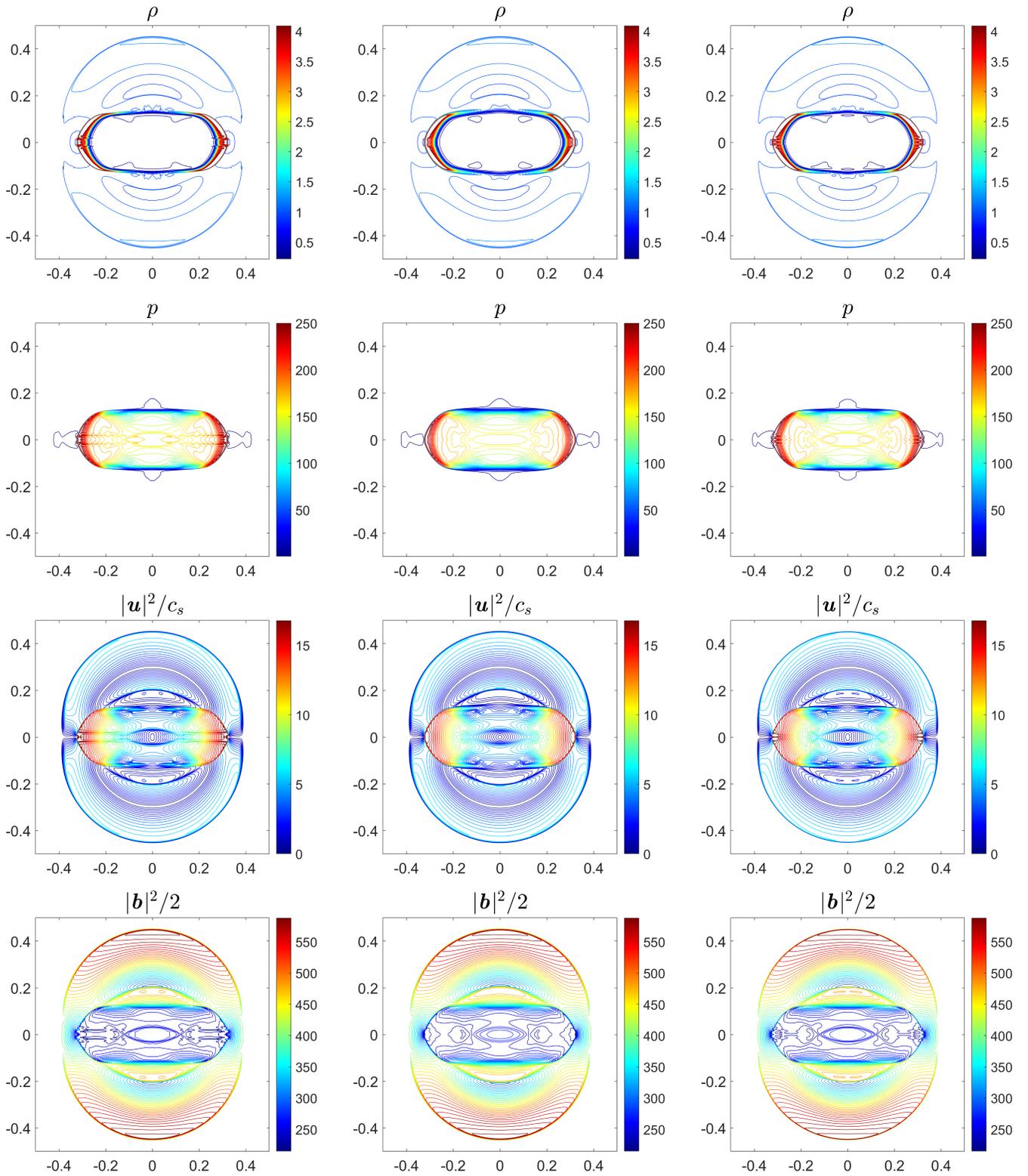


FIG. 4.9. Example 5: Density  $\rho$  (top row), pressure  $p$  (second row), velocity magnitude  $|u|$  (third row), and magnetic pressure  $|b|^2/2$  (bottom row) computed by the LCD-PCCU scheme on a uniform  $1000 \times 1000$  mesh (left column) and PCCU scheme on uniform  $1000 \times 1000$  (middle column) and  $2000 \times 2000$  (right column) meshes.

$\gamma_n := n - \gamma$  for  $n = 1, 2, 3$ , and

$$\begin{aligned} a_1 &:= -\frac{\gamma_3}{2}u_N^2 - \frac{\gamma_1}{2}(u_T^2 + w^2), & a_2 &:= u_N \left( \frac{\gamma_1}{2\rho} \left( \mathcal{E} + p + \frac{1}{2}|\mathbf{b}|^2 \right) |\mathbf{u}|^2 - \frac{b_N}{\rho} (\mathbf{u} \cdot \mathbf{b}) \right), \\ a_3 &:= \frac{1}{\rho} \left( \mathcal{E} + p + \frac{1}{2}|\mathbf{b}|^2 \right) - \frac{b_N^2}{\rho} + \gamma_1 u_N^2, & a_4 &:= \gamma_1 u_N u_T - \frac{1}{\rho} b_N b_T, & a_5 &:= \gamma_1 u_N w - \frac{1}{\rho} b_N b_3, \\ a_6 &:= \gamma_2 u_N b_T - u_T b_N, & a_7 &:= \gamma_2 u_N b_3 - w b_N. \end{aligned}$$

262 One can show that the eigenvalues of both  $C^x$  and  $C^y$  are given by

$$263 \quad (\text{A.3}) \quad \lambda_{1,8} = u_N \mp c_f, \quad \lambda_{2,7} = u_N \mp c_a, \quad \lambda_{3,6} = u_N \mp c_s, \quad \lambda_4 = \lambda_5 = u_N,$$

264 where

$$265 \quad (\text{A.4}) \quad c_a = \sqrt{\frac{b_N^2}{\rho}}, \quad c_{f,s} = \left[ \frac{1}{2} \left( c^2 + \frac{|\mathbf{b}|^2}{\rho} \pm \sqrt{\left( c^2 + \frac{|\mathbf{b}|^2}{\rho} \right)^2 - 4c^2 \frac{b_N^2}{\rho}} \right) \right]^{\frac{1}{2}},$$

266 and  $c := \sqrt{\gamma\rho/\rho}$  is the speed of sound.

267 Finally, we provide the formula for the matrices  $R^x$  and  $R^y$ , which diagonalize  $C^x$  and  $C^y$ , that is,  
268  $(R^x)^{-1}C^x R^x$  and  $(R^y)^{-1}C^y R^y$  are diagonal. One can show that  $R^x = [\mathbf{r}_1^x | \mathbf{r}_2^x | \dots | \mathbf{r}_8^x]$  and  $(R^x)^{-1} =$   
269  $[\boldsymbol{\ell}_1^x | \boldsymbol{\ell}_2^x | \dots | \boldsymbol{\ell}_7^x | \boldsymbol{\ell}_8^x]^\top$ , where  $\mathbf{r}_i^x$  and  $\boldsymbol{\ell}_i^x$ ,  $i = 1, \dots, 8$  are the right and left eigenvectors of  $C^x$ :

$$\begin{aligned} 270 \quad \mathbf{r}_{1,8}^x &= \begin{pmatrix} \alpha_f \\ \alpha_f(u_N \mp c_f) \\ \alpha_f u_T \pm \alpha_s \beta_1 \beta_2 c_a \\ \alpha_f w \pm \alpha_s \beta_1 \beta_3 c_a \\ \frac{1}{2} \alpha_f |\mathbf{u}|^2 + \mu_f^\mp \\ 0 \\ \frac{1}{\sqrt{\rho}} \alpha_s \beta_2 c_f \\ \frac{1}{\sqrt{\rho}} \alpha_s \beta_3 c_f \end{pmatrix}, \quad \mathbf{r}_{2,7}^x = \begin{pmatrix} 0 \\ 0 \\ \pm \beta_1 \beta_3 \\ \mp \beta_1 \beta_2 \\ \pm (\beta_3 u_T - \beta_2 w) \beta_1 \\ 0 \\ \frac{1}{\sqrt{\rho}} \beta_3 \\ -\frac{1}{\sqrt{\rho}} \beta_2 \end{pmatrix}, \quad \mathbf{r}_{3,6}^x = \begin{pmatrix} \alpha_s \\ \alpha_s(u_N \mp c_s) \\ \alpha_s u_T \mp \alpha_f \beta_1 \beta_2 c \\ \alpha_s w \mp \alpha_f \beta_1 \beta_3 c \\ \frac{1}{2} \alpha_s |\mathbf{u}|^2 + \mu_s^\mp \\ 0 \\ -\frac{1}{c_f \sqrt{\rho}} \alpha_f \beta_2 c^2 \\ -\frac{1}{c_f \sqrt{\rho}} \alpha_f \beta_3 c^2 \end{pmatrix}, \\ 271 \quad \mathbf{r}_4^x &= \left( 1, u_N, u_T, w, \frac{1}{2} |\mathbf{u}|^2, 0, 0, 0 \right)^\top, \quad \mathbf{r}_5^x = (0, 0, 0, 0, 0, 1, 0, 0)^\top, \quad \boldsymbol{\ell}_5^x = (0, 0, 0, 0, 0, 1, 0, 0)^\top, \\ 272 \quad \boldsymbol{\ell}_{1,8}^x &= \begin{pmatrix} \frac{1}{2} \theta_1 \alpha_f c^2 |\mathbf{u}|^2 \pm \theta_2 [\alpha_f c u_N \beta_1 - \alpha_s c_s (\beta_2 u_T + \beta_3 w)] \\ -\theta_1 \alpha_f c^2 u_N \mp \theta_2 \alpha_f c \beta_1 \\ -\theta_1 \alpha_f c^2 u_T \pm \theta_2 \alpha_s c_s \beta_2 \\ -\theta_1 \alpha_f c^2 w \pm \theta_2 \alpha_s c_s \beta_3 \\ \theta_1 \alpha_f c^2 \\ 0 \\ \theta_1 \sqrt{\rho} \alpha_s \beta_2 c_f \left( c_s^2 - \frac{\gamma_2}{\gamma_1} c^2 \right) \\ \theta_1 \sqrt{\rho} \alpha_s \beta_3 c_f \left( c_s^2 - \frac{\gamma_2}{\gamma_1} c^2 \right) \end{pmatrix}, \quad \boldsymbol{\ell}_{2,7}^x = \begin{pmatrix} \mp \frac{1}{2} \beta_1 (\beta_3 u_T - \beta_2 w) \\ 0 \\ \pm \frac{1}{2} \beta_1 \beta_3 \\ \mp \frac{1}{2} \beta_1 \beta_2 \\ 0 \\ 0 \\ \frac{1}{2} \sqrt{\rho} \beta_3 \\ -\frac{1}{2} \sqrt{\rho} \beta_2 \end{pmatrix}, \end{aligned}$$

$$273 \quad \ell_{3,6}^x = \begin{pmatrix} \frac{1}{2}\theta_1\alpha_s c_f^2 |\mathbf{u}|^2 \pm \theta_2 [\alpha_s c_a u_N \beta_1 + \alpha_f c_f (\beta_2 u_T + \beta_3 w)] \\ -\theta_1 \alpha_s c_f^2 u_N \mp \theta_2 \alpha_s c_a \beta_1 \\ -\theta_1 \alpha_s c_f^2 u_T \mp \theta_2 \alpha_f c_f \beta_2 \\ -\theta_1 \alpha_s c_f^2 w \mp \theta_2 \alpha_f c_f \beta_3 \\ \theta_1 \alpha_s c_f^2 \\ 0 \\ -\theta_1 \sqrt{\rho} \alpha_f \beta_2 c_f \left( c_f^2 - \frac{\gamma_2}{\gamma_1} c^2 \right) \\ -\theta_1 \sqrt{\rho} \alpha_f \beta_3 c_f \left( c_f^2 - \frac{\gamma_2}{\gamma_1} c^2 \right) \end{pmatrix}, \quad \ell_4^x = \begin{pmatrix} 1 - \theta_1 (\alpha_f^2 c^2 + \alpha_s^2 c_f^2) |\mathbf{u}|^2 \\ 2\theta_1 (\alpha_f^2 c^2 + \alpha_s^2 c_f^2) u_N \\ 2\theta_1 (\alpha_f^2 c^2 + \alpha_s^2 c_f^2) u_T \\ 2\theta_1 (\alpha_f^2 c^2 + \alpha_s^2 c_f^2) w \\ -2\theta_1 (\alpha_f^2 c^2 + \alpha_s^2 c_f^2) \\ 0 \\ 2\theta_1 \sqrt{\rho} \alpha_f \alpha_s \beta_2 c_f \left( c_f^2 - c_s^2 \right) \\ 2\theta_1 \sqrt{\rho} \alpha_f \alpha_s \beta_3 c_f \left( c_f^2 - c_s^2 \right) \end{pmatrix}.$$

Here,

$$\beta_1 := \text{sign}(b_N), \quad (\beta_2, \beta_3) := \begin{cases} \left( \frac{1}{\sqrt{2}}, \frac{1}{\sqrt{2}} \right), & \text{if } b_T = b_3 = 0, \\ \left( \frac{b_T}{\sqrt{b_T^2 + b_3^2}}, \frac{b_3}{\sqrt{b_T^2 + b_3^2}} \right) & \text{otherwise,} \end{cases}$$

$$(\alpha_f, \alpha_s) := \begin{cases} (1, 1) & \text{if } b_T = b_3 = 0, \\ \left( \sqrt{\frac{c_f^2 - c_a^2}{c_f^2 - c_s^2}}, \sqrt{\frac{c_f^2 - c^2}{c_f^2 - c_s^2}} \right) & \text{otherwise,} \end{cases}$$

$$\theta_1 := \frac{1}{2} \left[ \alpha_f^2 c^2 \left( c_f^2 - \frac{\gamma_2}{\gamma_1} c^2 \right) + \alpha_s^2 c_f^2 \left( c_s^2 - \frac{\gamma_2}{\gamma_1} c^2 \right) \right]^{-1}, \quad \theta_2 := \frac{1}{2} \left[ \alpha_f^2 c_f a \beta_1 + \alpha_s^2 c_s c_a \beta_1 \right]^{-1},$$

$$\mu_f^\mp := -\frac{\alpha_f c_f^2}{\gamma_1} \mp \alpha_f c_f u_N \pm \alpha_s c_a \beta_1 (\beta_2 u_T + \beta_3 w) + \frac{\gamma_2}{\gamma_1} \alpha_f (c_f^2 - c^2),$$

$$\mu_s^\mp := -\frac{\alpha_s c_s^2}{\gamma_1} \mp \alpha_s c_s u_N \mp \alpha_f c \beta_1 (\beta_2 u_T + \beta_3 w) + \frac{\gamma_2}{\gamma_1} \alpha_s (c_s^2 - c^2).$$

274 The structure of the matrices  $R^y$  and  $(R^y)^{-1}$  is similar, but in all of the right and left eigenvectors  
275 above, one needs to switch the second and third components as well as the sixth and seventh components.

276 **Appendix B. Eigendecomposition for Primitive Variables.** In this appendix, we provide the  
277 reader with the matrices used in the LCD for the quasi-linear system (2.10); see [34] for details.

278 First, the matrices  $D^x$  and  $D^y$  are

$$279 \quad D^x(\mathbf{V}) = \begin{pmatrix} u & \rho & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & u & 0 & 0 & \frac{1}{\rho} & 0 & \frac{b_2}{\rho} & \frac{b_3}{\rho} \\ 0 & 0 & u & 0 & 0 & 0 & -\frac{b_1}{\rho} & 0 \\ 0 & 0 & 0 & u & 0 & 0 & 0 & -\frac{b_1}{\rho} \\ 0 & \gamma p & 0 & 0 & u & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & u & 0 & 0 \\ 0 & b_2 & -b_1 & 0 & 0 & 0 & u & 0 \\ 0 & b_3 & 0 & -b_1 & 0 & 0 & 0 & u \end{pmatrix}$$

280 and

$$281 \quad D^y(\mathbf{V}) = \begin{pmatrix} v & 0 & \rho & 0 & 0 & 0 & 0 & 0 \\ 0 & v & 0 & 0 & 0 & -\frac{b_2}{\rho} & 0 & 0 \\ 0 & 0 & v & 0 & \frac{1}{\rho} & \frac{b_1}{\rho} & 0 & \frac{b_3}{\rho} \\ 0 & 0 & 0 & v & 0 & 0 & 0 & -\frac{b_2}{\rho} \\ 0 & 0 & \gamma p & 0 & v & 0 & 0 & 0 \\ 0 & -b_2 & b_1 & 0 & 0 & v & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & v & 0 \\ 0 & 0 & b_3 & -b_2 & 0 & 0 & 0 & v \end{pmatrix}.$$

282 We note that the matrices  $D^x$  and  $D^y$  have the same eigenvalues (A.3)–(A.4) as the matrices  $C^x$  and  
 283  $C^y$ , but different eigenvectors. The matrix  $T^x$ , which diagonalizes  $D^x$  is  $T^x = [\mathbf{r}_1^x | \mathbf{r}_2^x | \dots | \mathbf{r}_7^x | \mathbf{r}_8^x]$  and its  
 284 inverse is  $(T^x)^{-1} = [\boldsymbol{\ell}_1^x | \boldsymbol{\ell}_2^x | \dots | \boldsymbol{\ell}_7^x | \boldsymbol{\ell}_8^x]^\top$ , where  $\mathbf{r}_i^x$  and  $\boldsymbol{\ell}_i^x$ ,  $i = 1, \dots, 8$  are the right and left eigenvectors  
 285 of  $D^x$ :

$$286 \quad \mathbf{r}_{1,8}^x = \begin{pmatrix} \hat{\alpha}_f \rho \\ \mp \hat{\alpha}_f c_f \\ \pm \hat{\alpha}_s c_s \beta_1 \beta_2 \\ \pm \hat{\alpha}_s c_s \beta_1 \beta_3 \\ \hat{\alpha}_f \rho c^2 \\ 0 \\ \hat{\alpha}_s \sqrt{\rho} c \beta_2 \\ \hat{\alpha}_s \sqrt{\rho} c \beta_3 \end{pmatrix}, \quad \mathbf{r}_{2,7}^x = \begin{pmatrix} 0 \\ 0 \\ \mp \beta_3 \\ \pm \beta_2 \\ 0 \\ 0 \\ -\sqrt{\rho} \beta_1 \beta_3 \\ \sqrt{\rho} \beta_1 \beta_2 \end{pmatrix}, \quad \mathbf{r}_{3,6}^x = \begin{pmatrix} \hat{\alpha}_s \rho \\ \mp \hat{\alpha}_s c_s \\ \mp \hat{\alpha}_f c_f \beta_1 \beta_2 \\ \mp \hat{\alpha}_f c_f \beta_1 \beta_3 \\ \hat{\alpha}_s \rho c^2 \\ 0 \\ -\hat{\alpha}_f \sqrt{\rho} a \beta_2 \\ -\hat{\alpha}_f \sqrt{\rho} a \beta_3 \end{pmatrix},$$

$$287 \quad \mathbf{r}_4^x = (1, 0, 0, 0, 0, 0, 0, 0)^\top, \quad \mathbf{r}_5^x = (0, 0, 0, 0, 0, 1, 0, 0)^\top,$$

$$288 \quad \boldsymbol{\ell}_{1,8}^x = \frac{1}{2c^2} \begin{pmatrix} 0 \\ \mp \hat{\alpha}_f c_f \\ \pm \hat{\alpha}_s c_s \beta_1 \beta_2 \\ \pm \hat{\alpha}_s c_s \beta_1 \beta_3 \\ \frac{1}{\rho} \hat{\alpha}_f \\ 0 \\ \frac{1}{\sqrt{\rho}} \hat{\alpha}_s c \beta_2 \\ \frac{1}{\sqrt{\rho}} \hat{\alpha}_s c \beta_3 \end{pmatrix}, \quad \boldsymbol{\ell}_{2,7}^x = \frac{1}{2} \begin{pmatrix} 0 \\ 0 \\ \mp \beta_3 \\ \pm \beta_2 \\ 0 \\ 0 \\ -\frac{1}{\sqrt{\rho}} \beta_1 \beta_3 \\ \frac{1}{\sqrt{\rho}} \beta_1 \beta_2 \end{pmatrix}, \quad \boldsymbol{\ell}_{3,6}^x = \frac{1}{2c^2} \begin{pmatrix} 0 \\ \mp \hat{\alpha}_s c_s \\ \mp \hat{\alpha}_f c_f \beta_1 \beta_2 \\ \mp \hat{\alpha}_f c_f \beta_1 \beta_3 \\ \frac{1}{\rho} \hat{\alpha}_s \\ 0 \\ -\frac{1}{\sqrt{\rho}} \hat{\alpha}_f c \beta_2 \\ -\frac{1}{\sqrt{\rho}} \hat{\alpha}_f c \beta_3 \end{pmatrix},$$

$$289 \quad \boldsymbol{\ell}_4^x = \left(1, 0, 0, 0, -\frac{1}{c^2}, 0, 0, 0\right)^\top, \quad \boldsymbol{\ell}_5^x = (0, 0, 0, 0, 0, 1, 0, 0)^\top.$$

Here,

$$(\hat{\alpha}_f, \hat{\alpha}_s) = \begin{cases} \left(\frac{1}{\sqrt{2}}, \frac{1}{\sqrt{2}}\right) & \text{if } b_T = b_3 = 0, \\ \left(\sqrt{\frac{(c^2 - c_s^2)}{(c_f^2 - c_s^2)}}, \sqrt{\frac{(c_f^2 - c^2)}{(c_f^2 - c_s^2)}}\right) & \text{otherwise,} \end{cases}$$

290 and the other notations are the same as in Appendix A. The structure of the matrices  $T^y$  and  $(T^y)^{-1}$ ,  
 291 which diagonalize  $D^y$  is similar, but in all of the right and left eigenvectors above, one needs to switch  
 292 the second and third components as well as the sixth and seventh components.

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